

Unfortunately, the analysis of loading patterns of ISF-1 pool compartments shows that there is a significant amount of fuel that does not satisfy the conditions of loading curve (Fig. 5).

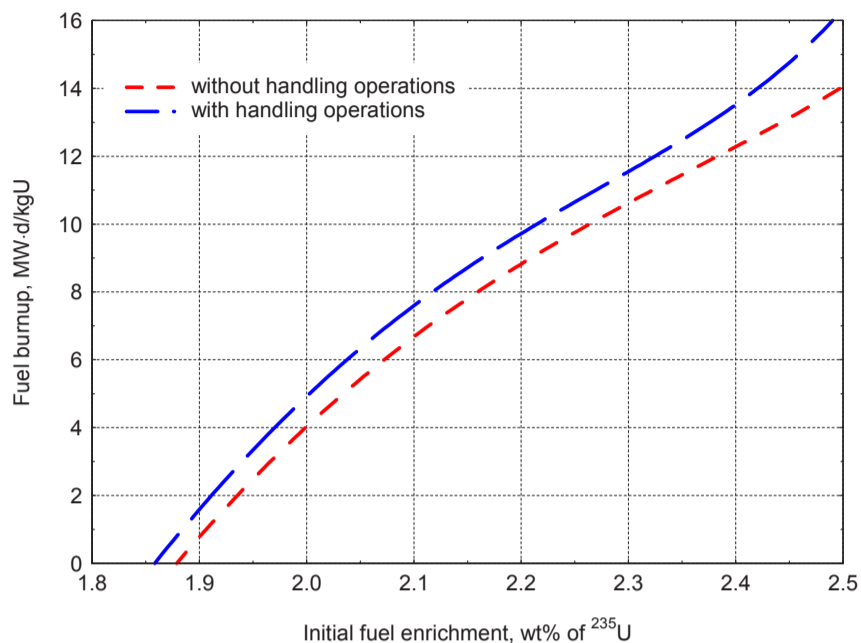


Fig. 5 – Loading curves for ISF-1 pool compartments

A procedure was developed for the criticality safety assessment of each pool compartment with burnup credit:

1) HELIOS code is used to calculate the isotopic composition of spent nuclear fuel from RBMK reactors at ChNPP.

2) In the analysis of ISF-1 criticality safety with burnup credit, change in the concentrations of the following five isotopes is considered:



3) Burnup credit is applied only for standard and regenerated fuel. For other types of spent fuel assemblies, it is assumed that the fuel is "fresh".

4) Non-uniformity of burnup distribution along the fuel length in criticality safety substantiation is taken into account by a conservative three-step burnup profile (Fig. 4, curve 4).

5) In view of a large number of cells with assemblies, all standard and regenerated spent fuel assemblies are divided into groups, having one of the five values of power release:

$$0, \quad 470, \quad 940, \quad 1400, \quad 1870 \text{ MW}\cdot\text{d}/\text{FA}.$$

### Result of the implementation of burnup credit for nuclear safety analysis of ISF-1 compartments

For optimal distribution of the moderator (steam-water mixture) in the system, the maximum

effective neutron multiplication factor excluding fuel burnup is [1]:

$$K_{\text{eff}} \pm \sigma = 1.02652 \pm 0.00046.$$

Considering the optimal neutron moderation, for a conservative load pattern of the ISF-1 compartment, the effective neutron multiplication factor obtained with fuel burnup credit is equal to:

$$K_{\text{eff}} + 3\sigma = 0.9392.$$

Taking into account handling operations in the compartment and conservatively assuming that each row in the transportation corridor between halves of rows has a canister with a fresh fuel assembly with the highest multiplication properties, the neutron multiplication factor is:

$$K_{\text{eff}} + 3\sigma = 0.9447.$$

### Conclusions

A more realistic assessment of criticality safety, based on the calculations of  $K_{\text{eff}}$  with burnup credit improves the situation and proves compliance with the regulations of Ukraine,  $K_{\text{eff}} < 0.95$ .

### References

1. Safety Analysis Report for Interim Spent Fuel Storage Facility 1. Revision 3.00 (in Russian).
2. Y. Bilodid, Y. Kovbasenko, et al. Introducing a burnup credit methodology in nuclear safety analysis practice in Ukraine. Proceedings of Int. Conference "Radioactive Waste and Spent Fuel Management", Plovdiv, Bulgaria, November 6-8, 2003.
3. O. Dudka, Y. Bilodid, et al. Use of the axial burnup profile at the nuclear safety analysis of the VVER-1000 spent fuel storage in Ukraine. Proceedings of 17<sup>th</sup> Symposium of AER on VVER Reactor Physics and Reactor Safety. Yalta, Crimea, Ukraine. September 24-29, 2007
4. Y. Bilodid, O. Dudka, Yu. Kovbasenko. Interim dry spent fuel storage facility at Zaporizhzhya NPP. Proceedings of Regional Workshop on Spent Fuel Cask/Container Design. Bucharest, Romania, 17-19 October 2011,
5. A. V. Krayushkin. Development and implementation of transient mathematical models of the RBMK reactor. Thesis for the degree of Doctor of Technical Sciences. Scientific and Research Center "Kurchatov Institute", Moscow, 2007 (in Russian).